

STRENGTH PROPERTIES ESTIMATION OF FROZEN ROCKS BY LOGGING DATA

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Geological situation of the South-Yakutian coal-field is complex due to geocryological factors, e.g. overall development of insular permafrost.

Strength and indexes of permafrost rock are increasing for 30% at an average. Natural gamma-intensity I_γ does not undergo practical changes in the process of epigenetic transformation of rock and cryogenic processes. Consequently, gamma-ray logging data (GL) present the opportunity to evaluate argillaceousness and lithologic composition, which have dominating effect on strength property of rock.

The structure and texture characteristic properties of the section are being evaluated by the data of borehole gauging. Data of borehole diameter variation during the drilling process may be regarded integral characteristic of rock strength.

Using multimeasuring correlations between geophysic parameters I_γ , δv and strength properties of rock σ_{cm} and σ_t , are being studied the strength properties of permafrosted coal-containing rock by the finding of logging.

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In conditions of application of modern highly mechanized mining and drifting complexes in construction and exploitation of coal mining industry pits, demands for studies of strength properties of rock have been increasing.

Studies of strength of rock by means of core testing laboratory methods have number of essential disadvantages.

1. Testing is being provided optionally on sections of discrete boreholes, e.g. over the optional network.

2. Being drilled, mechanically soft rock is breaking and it is hardly possible to extract core from them. As a result, for strength property analysis only those cores are being tested in laboratory, which happened to hold their shape sufficiently. It results in artificial increase of strength indexes of the section, while soft rock, bedding in roof and seam floor of coal seam, are considered the most important subject of the research.

In order to enhance the validity of strength prognosis of rock and efficiency of coal exploration in the conditions of permafrost rock, within the South-Yakutian coal field there have been used to special technique, defining the strength of permafrost rock due to their natural state.

The South-Yakutian coal-field is the main base of coking coal in the East of Russia. The area of coal field within the borders of development of mezozoic coal bearing deposits constitutes 26 thousand square kilometers.

Coalbearing deposits are being presented by monotonic considerably transformed aleuro-sand rock, which is referred, according to petrophysical classification of professor V.V.Grechukhin, to VIII - XI stages of coal bearing deposit transformation [1].

Geological situation of the field is complex due to geocryological factors, e.g. overall development of insular permafrost. Permafrost rock have intermittent spread by area and entire spread by vertical. The thickness of permafrosted rock varies from the first meters up to 200 meters.

In general, there is a range of the temperature variation of permafrost rock from 0°C to -4°C within present coal field. Permafrosted seams with temperature from 0°C to -2°C are widespread. The thickness of seasonal frost penetration varies from 1.5-2 meters.

Strength, as well as physical properties have been formed under the influence of both

groups of factors: primary (genetic) and secondary process of rock transformation.

There is a number of factors attributed to the primary factors: material and grain-size analysis, texture, structure, primary material attribution, type and composition of cement, organic impurities [1].

By the feature of material composition coalbearing rock can be divided into clay, carbonate and fragmental rocks. Of all these rocks, clay rock have the lowest strength properties, while carbonate rock and silicified fragmental rock have the highest strength index.

Strength properties of rock are being considerably affected by the cement of this rock. Rocks with carbonate cement or secondary silicification are specified by high index strength properties. Increase of clay cement content in rock is accompanied by decrease in strength properties.

Structure and texture characteristic properties of rock have considerable effect on strength of rock. Usually thin lamination of rocks reduces their strength, especially if there are interlayers of coal argillite. There is an increase in jointing of thin laminated rock, which evokes additional reduction of rock strength [2, 4].

The secondary factors affecting rock strength are processes of diagenesis, epigenesis and metagenesis appearing under the affect of overlapping rock mass pressure and temperature, determined by geothermal gradient and particular paleodepth [1].

With submersion of rock the density increase and porosity decrease take place, accompanied by increase of volume density, elastic wave propagation velocity, increase of strength and deformation properties. These kinds of transformation are irreversible. Therefore, physical and chemical properties of rocks are being specified by the indexes attained at maximum pressure and temperature values, i.e. at the maximum depth of their submersion. Subsequent raise of rock do not cause changes in physical and chemical properties. Established associations and mechanisms become violated in zones with

widespread permafrost rock. In comparison with those of thawed rock, strength and elasticity indexes of permafrost rock are increasing by 30% on an average. The difference of physical properties between different lithologic types of permafrost enclosing rocks and coal is considerably reducing. Cryogenic processes do not influence volume density and magnetic susceptibility. Natural gamma-intensity I_γ does not undergo practical changes in the process of epigenetic transformation of rock and cryogenic processes, while the rest of the mentioned parameters (Table 1) are changing.

Consequently, gamma-ray logging data (GL) present the opportunity to evaluate argillaceousness and lithologic composition, which have dominating effect on strength property of particular rock that constitute sections of boreholes in permafrost rock.

For more precise definition of lithologic composition and zones of broken rock, there is a logging of magnetic susceptibility to be used (LMS), as far as magnetic susceptibility of rock is not affected by cryogenic processes [3].

The structure and texture characteristic properties of the section are being evaluated by the data of borehole gauging. Data of borehole diameter variation during the drilling process may be regarded as an integral characteristic of rock strength.

By the feature of borehole diameter variation during drilling, coalbearing rocks can be divided into two types.

Attributed to the first type are those rocks (dense carbonate sandstone, conglomerate, silicified sandstone), where borehole diameter practically does not deviate from rated.

Attributed to the second type are most of rock (bituminous coal, argillite, argillaceous sandstone), which being drilled through collapse boreholes, diameters increase by 1.3-1.8 times, and there are cavities formed on some borehole intervals with virtual diameter δv , that is exceeding rated borehole diameter 2-3 times.

Table 1

Average values of physical and mechanical properties of the frozen rock in the South-Yakutian coal field (Elga's coal deposit)

Phys.-mech. Properties	Coarse grained sandstone		Medium grained sandstone		Fine drained sandstone		Aleurolits		Coal A ^d = 15% absolute	
	thawed	permafrosted	thawed	permafrosted	thawed	permafrosted	thawed	permafrosted	thawed	permafrosted
V _p , m/s	4100	5000	4570	5200	4700	5600	2850	4500	2200	3500
ρ, Ωm	750	4950	450	2930	275	1520	150	1200	7500	9000
I _γ , pA/kg	0.5	0.5	0.72	0.72	0.86	0.86	1.08	1.08	0.36	0.36
χ × 10 ⁻⁵ unit CI	8	8	12	12	18	18	38	38	3	3
δv, g/sm ³	2.45	2.45	2.58	2.58	2.63	2.62	2.61	2.61	1.37	1.37
σ _{cm} , mPa	57	79	65	87	72	91.3	50	72	-	-
σ _t , mPa	6.3	9.2	7.8	11.0	10.3	12.1	6.7	9.9	-	-

Note: thawed - t > 0⁰ C, permafrosted 0⁰ > t < -4⁰C, elastic wave propagation velocity, ρ - electrical resistance, I_γ - natural radioactivity, χ - magnetic susceptibility, δ_v - volume density, σ_{cm}, σ_t - compression and tensile strength limits.

Therefore, relationship of borehole diameter variation with the lithologic composition of rock in the drilling process is to be observed.

From the borehole gauging data analysis, it follows that with the identical conditions of drilling there is an extension of borehole diameter to be observed: a) with the increase of organic impurity content in rock; b) with the increase of argillaceous cement content; c) with the decrease of carbonate cement content, all these factors are being effected on gamma-ray logging diagram by increase or decrease of natural gamma γ - intensity.

With the same conditions, there is a change of uniaxial compression strength σ_{cm} and uniaxial tensile strength σ_t to take place.

Therefore, variation of natural radioactivity of rocks and borehole diameter depend on rock strength, and utilizing multimeasuring correlations between geophysic parameters I_γ, δv and strength properties of rock σ_{cm} and σ_t, it gives the possibility to study with certain precision the strength properties of permafrosted coalcontaining rock by the finding of logging.

For the approximating function the following exponential function is to be chosen:

$$y_i = \sum_{i=n}^n C_i \cdot 10^{a_{i0} + a_{i1}x_{i1} + a_{i2}x_{i2} \dots} \quad (1)$$

where y_i - one of the strength parameters;
 x_{i1}, x_{i2} - geophysic parameters;
 a_{i0} - a_{i2} - polynomial coefficient;

Type of the function (1) has been chosen on the basis of regression analysis of strength parameters of diffrent lithologic types. Coefficients of the equation (1) for the definite coal field are being calculated by the method of least squares, with utilization of

particular ultimate strength values obtained in laboratory by core testing.

Thus, for Elga coal deposit there are following equations of evaluation σ_{cm} and σ_t of permafrosted coal rock:

$$\sigma_{cm} = 0.4605 \times 10^{\frac{4.1 - d_y - 0.5\Delta H^{0.63}}{d_r}} + 0.4605 \times 10^{-2.3\Delta I_y + 3.1} \quad (2)$$

$$\sigma_{cm} = 0.5 \times 10^{\frac{3.1 - d_y - 0.5\Delta H^{0.63}}{d_r}} + 0.5 \times 10^{-2.3\Delta I_y + 2.1} \quad (3)$$

where ΔH - difference between borehole depth and depth of virtual measurement being conducted.

I_r - normalized value of natural radioactivity, in relative units;

δ_r, δ_v - rated and virtual borehole diameters

Reliability of evaluation of strength by logging finding was checked by being compared with the results of laboratory core testing.

There is percentage root-mean-square error of strength property evaluation: for σ_{cm} - $\delta = 13\%$, for σ_t - $\sigma = 11\%$.

References

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